

High-Performance Numerical Simulation of Biodegradation Process with Moving Boundaries

FreeFEM Days, 11th Edition

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0 Our Research Group

- Supervisor: Prof. Ir. Liesbet Geris
- Research profile:

Computational Tissue Engineering, Computational Biomechanics, Computational Biology, Computational Genomics



1 Outline

Introduction

2 Mathematical Model

3 Computational Model and Parallelization

O Simulation Results

6 Performance Analysis



1 Reaction-Diffusion Systems with Moving Boundaries

- Stefan problems
- Diffusion-controlled interface
- Diffusion and reaction lead to the change of domain geometry
- Degradation is an example of such a system

1 Biodegradation Process

- Dissolution of the bulk material
- Formation of a protective film
- Effect of ions in the medium





1 A Sample Application

- Hip joint replacement implants
- Tuning the degradation parameters to the rate of bone growth





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2 Chemistry of Biodegradation

Some of the chemical reactions:

$$Mg \rightarrow Mg^{2+} + 2e^{-}$$

 $2H_2O+2e^- \rightarrow H_2+2OH^-$

 $\mathrm{Mg}^{2+} + 2\mathrm{OH}^{-} \xrightarrow{k_1} \mathrm{Mg}(\mathrm{OH})_2$



 $Mg(OH)_2 + 2Cl^- \xrightarrow{k_2} Mg^{2+} + 2Cl^- + 2OH^-$



2 Reaction-Diffusion Equations

$$C_{\text{Mg}} = C_{\text{Mg}}(x, t), \quad C_{\text{Film}} = C_{\text{Film}}(x, t) \quad x \in \Omega \subset \mathbb{R}^3$$

$$\frac{\partial C_{\mathrm{Mg}}}{\partial t} = \nabla \bullet \left(D_{\mathrm{Mg}}^{e} \bullet \nabla C_{\mathrm{Mg}} \right) - k_1 C_{\mathrm{Mg}} \left(1 - \frac{C_{\mathrm{Film}}}{[\mathrm{Film}]_{\mathrm{max}}} \right) + k_2 C_{\mathrm{Film}} [\mathrm{Cl}]^2$$

$$\frac{\partial C_{\text{Film}}}{\partial t} = k_1 C_{\text{Mg}} \left(1 - \frac{C_{\text{Film}}}{[\text{Film}]_{\text{max}}} \right) - k_2 C_{\text{Film}} [\text{Cl}]^2$$

$$D_{\rm Mg}^e = D_{\rm Mg} \left(\left(1 - \frac{C_{\rm Film}}{[\rm Film]_{\rm max}} \right) + \frac{C_{\rm Film}}{[\rm Film]_{\rm max}} \frac{\epsilon}{\tau} \right)$$

2 Level Set Method

Implicit signed distance function $\phi = \phi(x, t)$ $x \in \Omega \subset \mathbb{R}^3$



2 Coupling Mass Transfer and Level Set

$$\frac{\partial \phi}{\partial t} + \mathbf{v} |\nabla \phi| = 0$$

Rankine-Hugoniot:

$$\{\mathbf{J}(x,t) - (c_{\rm sol} - c_{\rm sat}) \mathbf{v}(x,t)\} \cdot n = 0$$

$$D_{\mathrm{Mg}}^{e} \nabla_{n} C_{\mathrm{Mg}} - ([\mathrm{Mg}]_{\mathrm{sol}} - [\mathrm{Mg}]_{\mathrm{sat}}) \mathbf{v} = 0$$

$$\frac{\partial \phi}{\partial t} - \frac{D_{\mathrm{Mg}}^{e} \nabla_{n} C_{\mathrm{Mg}}}{[\mathrm{Mg}]_{\mathrm{sol}} - [\mathrm{Mg}]_{\mathrm{sat}}} |\nabla \phi| = 0$$



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3 Weak Formulation

Rewriting the diffusion-reaction PDE:

$$\frac{\partial u}{\partial t} = \nabla \bullet (D \bullet \nabla u) - k_1 a u + k_2 p q^2$$

Defining trial and test function space:

$$\mathcal{S}_t = \left\{ u(\mathbf{x}, t) | \mathbf{x} \in \Omega, t > 0, u(\mathbf{x}, t) \in \mathcal{H}^1(\Omega), \text{ and } \frac{\partial u}{\partial n} = 0 \text{ on } \Gamma \right\}$$

$$\mathcal{V} = \left\{ v(\mathbf{x}) | \mathbf{x} \in \Omega, v(\mathbf{x}) \in \mathcal{H}^1(\Omega), \text{ and } v(\mathbf{x}) = 0 \text{ on } \Gamma \right\}$$

3 Weak Formulation cont.

$$\frac{\partial u}{\partial t}v = \nabla \bullet (D \bullet \nabla u)v - k_1 buv + k_2 pq^2 v \quad \forall v \in \mathcal{V}$$

Integrate over the whole domain:

$$\int_{\Omega} \frac{\partial u}{\partial t} v d\omega = \int_{\Omega} \nabla \bullet (D \bullet \nabla u) v d\omega - \int_{\Omega} k_1 b u v d\omega + \int_{\Omega} k_2 p q^2 v d\omega$$

Integration by part, Green's divergence theory, Backward Euler scheme:

$$\int_{\Omega} \frac{u - u^n}{\Delta t} v d\omega = \int_{\Gamma} Dv \bullet \frac{\partial u}{\partial n} d\gamma - \int_{\Omega} D \bullet \nabla u \bullet \nabla v d\omega - \int_{\Omega} k_1 b u v d\omega + \int_{\Omega} k_2 p q^2 v d\omega$$



3 Weak Formulation cont.

$$\int_{\Omega} uvd\omega + \int_{\Omega} \Delta tD \bullet \nabla \bullet u\nabla vd\omega + \int_{\Omega} \Delta tk_1 buvd\omega = \int_{\Omega} u^n vd\omega + \int_{\Omega} \Delta tk_2 pq^2 vd\omega$$

By defining a linear functional $(f,v) = \int_\Omega f v d\omega$

$$(u,v)[1 + \Delta tk_1b] + \Delta t(D\nabla u, \nabla v) = (u^n, v) + \Delta t(f^n, v)$$

multiplying to a new coefficient $\alpha = \frac{1}{1 + \Delta t k_1 b}$

$$(u,v) + \alpha \Delta t (D\nabla u, \nabla v) = \alpha (u^n, v) + \alpha \Delta t (f^n, v)$$



3 Discretization Scheme

$$\mathcal{V}_{h} = \operatorname{span}\left(\left\{\psi_{i}\right\}_{i\in\mathcal{I}_{s}}\right) \quad \mathcal{I}_{s} = \left\{0,\ldots,N\right\}$$

Using 1st order Lagrange polynomials as basis functions

$$u = \sum_{j=0}^{N} c_j \psi_j(\boldsymbol{x}), \quad u^n = \sum_{j=0}^{N} c_j^n \psi_j(\boldsymbol{x})$$

$$\sum_{j=0}^{N} \left(\psi_i, \psi_j\right) c_j + \alpha \Delta t \sum_{j=0}^{N} \left(\nabla \psi_i, D\nabla \psi_j\right) c_j = \sum_{j=0}^{N} \left(\psi_i, \psi_j\right) c_j^n + \Delta t \left(f^n, \psi_i\right)$$

3 Discretization Scheme cont.

A linear system of equations

$$\sum_{j} A_{i,j} c_j = b_i$$

$$A_{i,j} = (\psi_i, \psi_j) + \alpha \Delta t \left(\nabla \psi_i, D \nabla \psi_j \right)$$

$$b_{i} = \sum_{j=0}^{N} \alpha \left(\psi_{i}, \psi_{j}\right) c_{j}^{n} + \alpha \Delta t \left(f^{n}, \psi_{i}\right)$$



3 Discretization Scheme cont.

Final form as implemented in FreeFEM

$$(M + \alpha \Delta t K)c = \alpha M c_1 + \alpha \Delta t f$$

$$M = \{M_{i,j}\}, \quad M_{i,j} = (\psi_i, \psi_j), \quad i, j \in \mathcal{I}_s$$

$$K = \{K_{i,j}\}, \quad K_{i,j} = (\nabla \psi_i, D\nabla \psi_j), \quad i, j \in \mathcal{I}_s$$

$$f = \{f_i\}, \quad f_i = (f(\mathbf{x}, t_n), \psi_i), \quad i \in \mathcal{I}_s$$

$$c = \{c_i\}, \quad i \in \mathcal{I}_s$$

$$c_1 = \{c_i^n\}, \quad i \in \mathcal{I}_s$$



3 Level Set Implementation

- Penalization for interface BCs
- Computing $\nabla_n C_{\mathrm{Mg}}$ correctly
- Problem of oscillation
- ► Too flat or too steep gradients
- Nightmare of re-distancing



(P. Bajger et al. 2017)



3 Computational Mesh

- Eulerian mesh
- Generated using Netgen in SALOME platform
- Adaptively refined on the moving interface



3 Parallelization

- Message Passing Interface
- Distributed numerical integration (assigning a number in the range of [0, MPI Size-1] to each element)
- MUMPS multifrontal direct solver

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4 Release of lons and Degradation - Simple Screw



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4 Film Formation - Simple Screw



Formation of the protective film on the interface of material-medium



4 Release of lons and Degradation - Porous Structure



Trimmed view of the computational mesh



Formation of the protective film



4 Quantitative Results

Measuring mass loss:

- Direct weight reduction
- Side products evolution

Using level set output for calculating mass loss

$$Mg_{lost} = \int_{\Omega_{+}(t)} Mg_{solid} dV - \int_{\Omega_{+}(0)} Mg_{solid} dV_{0}$$
$$\Omega_{+}(t) = \{\mathbf{x} : \phi(\mathbf{x}, t) \ge 0\}$$





Simulation and experimental setup



4 Mass Loss and Evolving Side Products



Film formation and the comparison of predicted and experimental mass loss, measured by the evolved hydrogen gas



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5 Problem Size

- Same setup as the model for calibration and validation
- ▶ DOF: 144k
- Elements: 831k (P1)





5 Domain Decomposition



Two different approaches for domain decomposition. Colors show different mesh regions assigned to different MPI cores.



Execution time per time step

5 Weak-Scaling Test Results





Solving level set PDE Solving Mg PDE Solving film PDE



5 Weak-Scaling Test Analysis

Based on Gustafson's law:

Speedup =
$$f + (1 - f) \times N$$

Serial proportion = 86%, Parallelizable proportion = 14%



5 Strong-Scaling Test Results



Solving level set PDE Solving Mg PDE Solving film PDE Time required to solve each PDE in each time step



5 Strong-Scaling Test Analysis

Based on Amdahl's law:

Speedup =
$$\frac{1}{f + \frac{1-f}{N}}$$

Serial proportion = 52%, Parallelizable proportion = 48%





5 Conclusion

- A quantitative mathematical model and its corresponding computational model to assess the degradation behavior of biodegradable materials
- Using level set method to track the moving corrosion front during degradation
- Once fully validated, the model will be an important tool to find the right design and properties of the metallic biomaterials and implants

Thank you for your attention

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